

Simulation of Hydrogen Dispersion under Cryogenic Release Conditions

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OUTLINE

- Objectives
- Physics of LH2 dispersion
- Description of experiments
- Modeling Strategy
- Results
- Conclusions
- Future work



OBJECTIVES

- Define safety zones in case of an accidental release of **liquefied** hydrogen (LH2) using CFD tools
 1. Understand physics of LH2 dispersion
 2. Develop the CFD code
 3. Validate the code
 4. Use CFD code for prediction in similar cases



Validation of the ADREA-HF CFD code for cryogenic releases using the HSL experiments.



Physics of LH2 dispersion

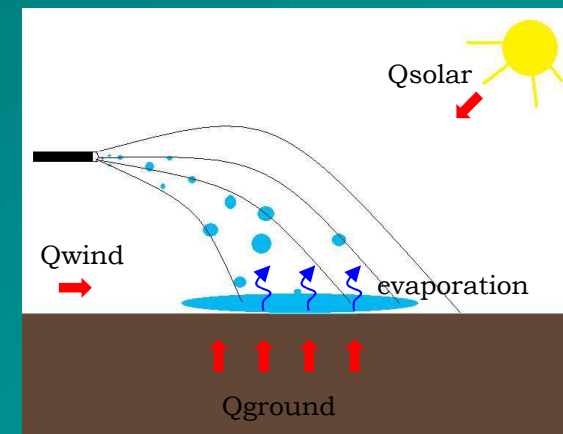
Two phase release \longrightarrow Two phase flow (vapor and droplets)
+ cryogenic pool is formed

During LH2 release:

- Cold cloud – Negative buoyancy
- Heat absorbing by the surrounding – Positive buoyancy

Factors that influence H2 dispersion:

- Release conditions
- Terrain features
- Atmospheric conditions
- Weather **conditions** (ambient temperature, ambient **humidity** wind velocity, **direction** etc.)
- Heat transfer from the ground





Physics of LH2 dispersion

Presence of Humidity



Condensation \ Solidification



Heat liberation

Droplet and Ice crystals

- Air
 - Vapor H_2
 - Vapor H_2O
 - Liquid H_2
 - Liquid H_2O
 - Solid H_2O
- } Non vapor phase





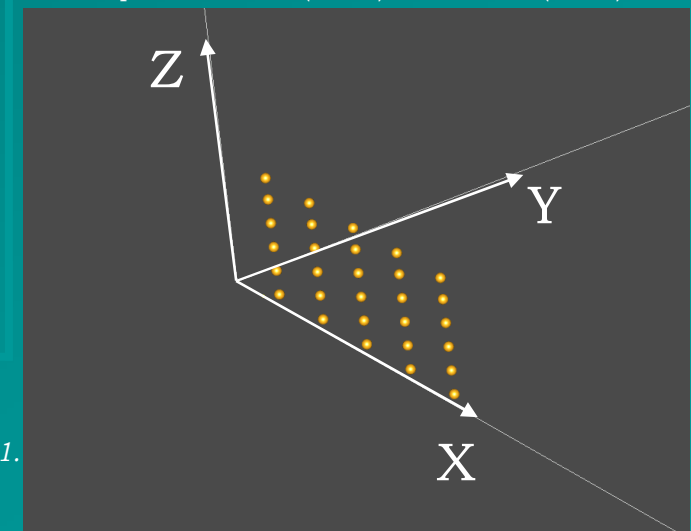
Description of Experiments

Release and Weather Conditions for the simulating tests ¹

Data	No test	5	6	7
spill rate (kg/sec)		0.07	0.07	0.07
spill diameter (mm)		26.6	26.6	26.6
source height (mm)		on ground (3.36)	100	860
source direction		Horizontal (x-direction)	Vertical (z-direction)	Horizontal (x-direction)
release duration (sec)		248	556	305
average wind speed (@2.5m) (standard deviation)		2.675 0.09	3.36 0.95	3.07 0.82
average wind direction (@2.5m) (standard deviation)		291 15.5	295 13.4	294.5 14
average ambient temperature (@2.5m)		283	283	283
ambient relative humidity (%)		68	68	64



Experimental site (above) and sensors (below)



¹ Hooker, P., Willoughby, D.B. and Royle, M., Example, Experimental Releases of Liquid Hydrogen, 4th International Conference on Hydrogen Safety, San Francisco, Paper 160, 2011.



MODELING STRATEGY

- Conservation equations: ~~Non-Hydrodynamic Equilibrium Model~~ (slip terms)

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_i}{\partial x_i} = 0$$

$$\frac{\partial \rho u_i}{\partial t} + \frac{\partial \rho u_j u_i}{\partial x_j} = -\frac{\partial p}{\partial x_i} + \frac{\partial}{\partial x_j} \left((\mu + \mu_t) \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \right) + \rho g_i - \delta_{3i} \frac{\partial}{\partial z} (\rho q_{nv} w_s (1 - q_{nv}) w_s)$$

$$\frac{\partial \rho q_k}{\partial t} + \frac{\partial \rho u_j q_k}{\partial x_j} = \frac{\partial}{\partial x_j} \left(\frac{\mu_t}{Sc_t} \frac{\partial q_k}{\partial x_j} \right) - \frac{\partial \rho q_{nv} w_s (1 - q_k)}{\partial z}$$

$$\frac{\partial \rho H}{\partial t} + \frac{\partial \rho u_j H}{\partial x_j} = \frac{\partial}{\partial x_j} \left(\frac{\mu_t}{Pr_t} \frac{\partial H}{\partial x_j} \right) + \frac{Dp}{Dt} + \frac{\partial}{\partial z} [\rho q_{nv} w_s (H - H_{nv})] - q_{nv} w_s \left(1 - \frac{\rho}{\rho_{nv}} \right) \frac{\partial P}{\partial z}$$

- ~~Slip distribution:~~ ^{Non-vapor phase} ~~Non-vapor phase~~ of component-I appears when the mixture temperature falls below the mixture dew temperature, which is calculated using the Raoult's law for ideal gases. The solid phase of component-I appears when the mixture temperature drops below the freezing point.
- Standard k-ε with buoyancy effect term.
- One dimensional, transient energy (temperature) equation inside the ground. The ground consists of two layers (an upper concrete layer and a sand layer on the bottom).

² Ogura Y. and Takahashi T., Numerical Simulation of the Life Cycle of a Thunderstorm Cell, Monthly Weather Review Journal, 99, 1971, pp. 895-911



MODELING STRATEGY

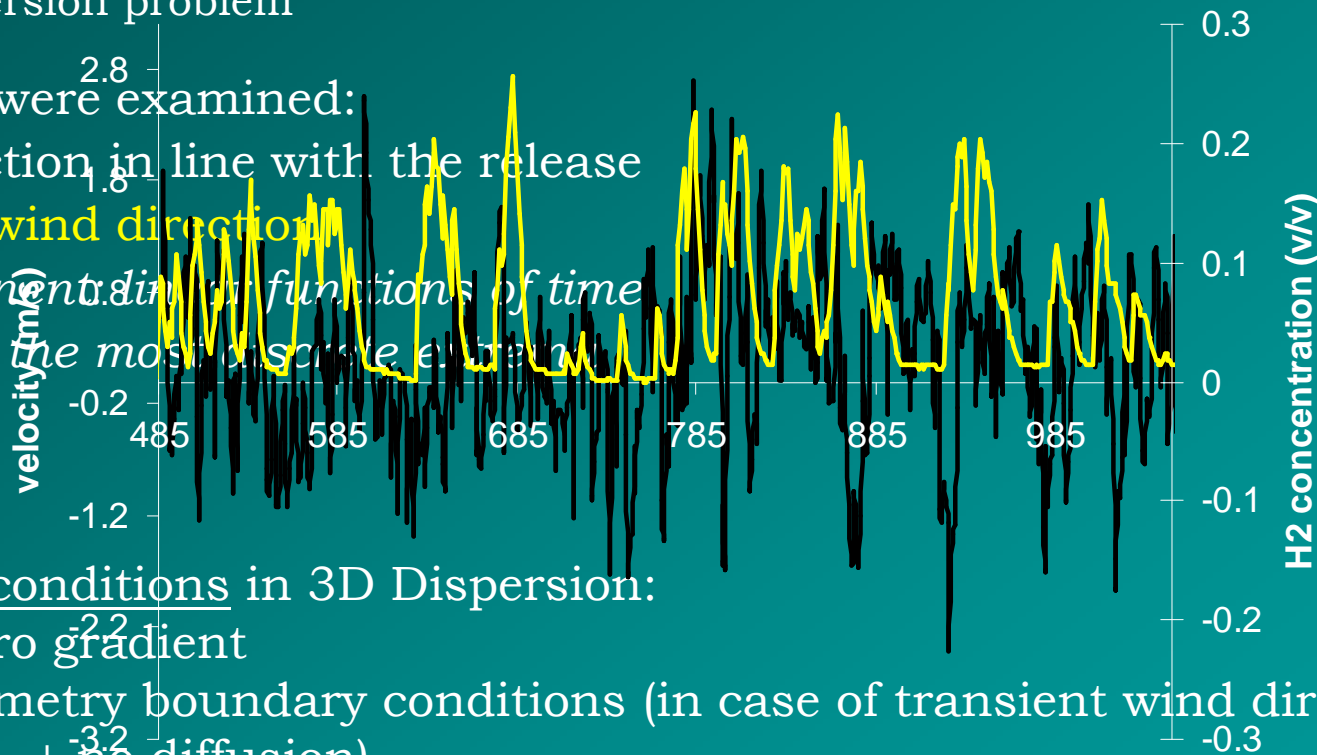
Simulation process:

1. 1D wind field
2. 3D Dispersion problem

Two cases were examined:

- wind direction in line with the release
- transient wind direction

v-component and H₂ concentration as functions of time between the most discrete elements



Boundary conditions in 3D Dispersion:

Outlet – zero gradient

Side – symmetry boundary conditions (in case of transient wind direction given value + no diffusion)

Source: velocity 6.06m/s, temperature 291 K, vapor mass fraction 71.34%

Test 6 - vertical release

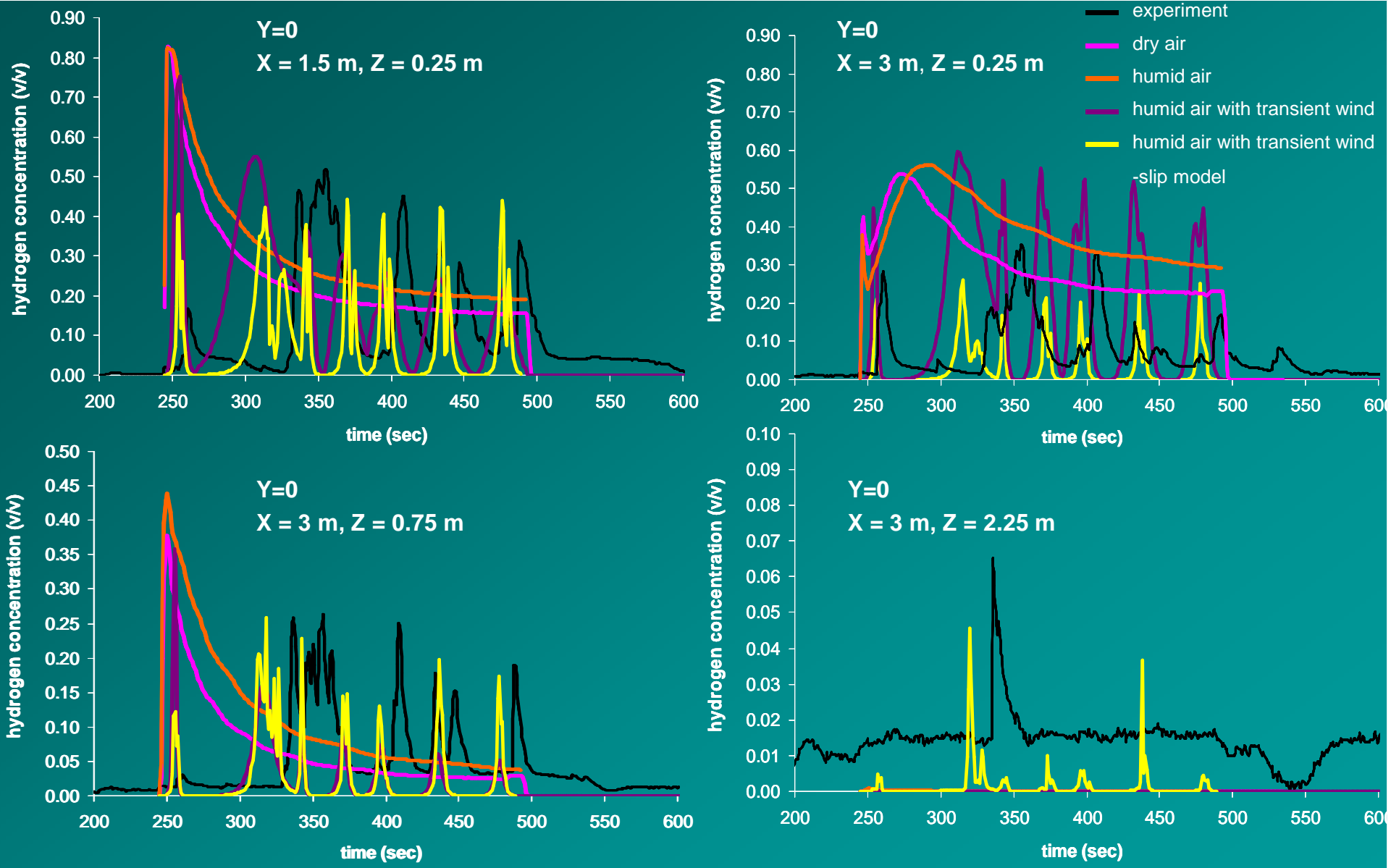


MODELING STRATEGY

	Computational domain (m) (x, y, z)	Grid Characteristic (m)				
		grid dimension	total number of cells	dx min	dy min	dz min
Test5	(15, 20, 10)	40 x 69 x 34	93 840	0.1	0.027	0.027
Test6	(15, 20, 10)	63 x 68 x 28	119 952	0.027	0.027	0.05
Test7	(25, 20, 10)	45 x 69 x 49	152 145	0.1	0.027	0.027

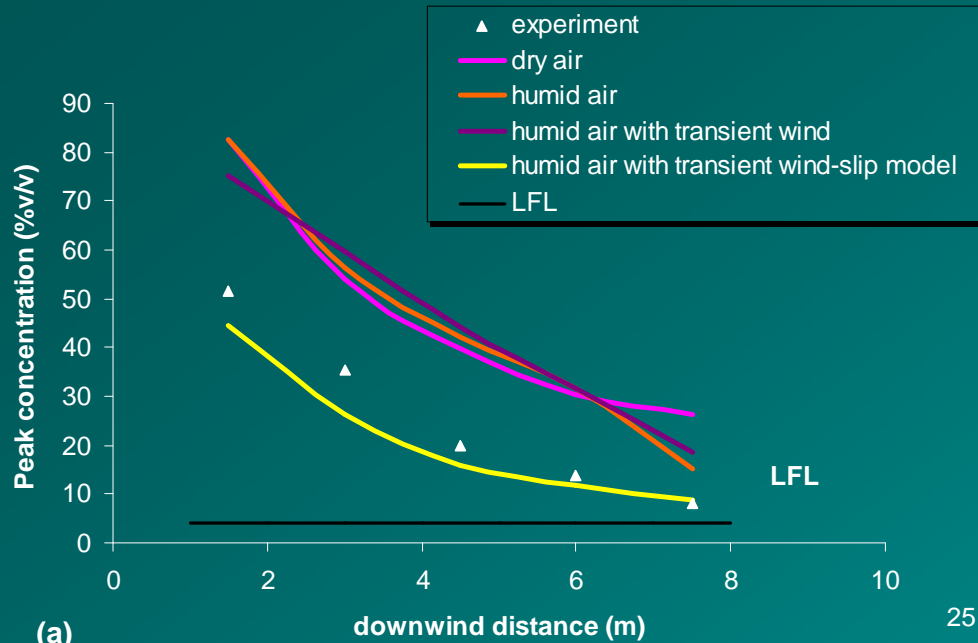


RESULTS (TEST 5)





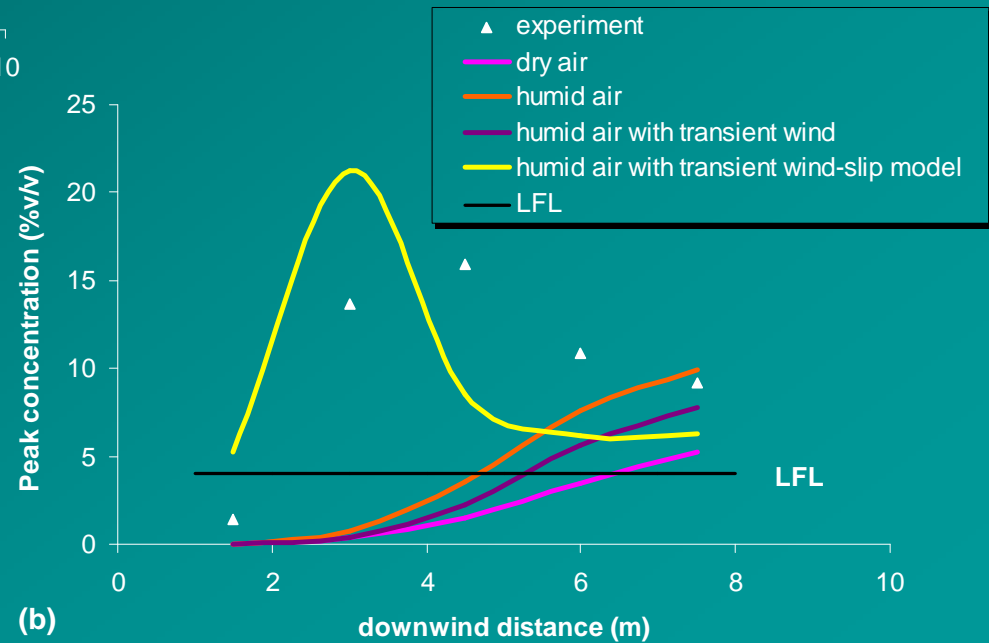
RESULTS (TEST 5)



↔ 0.25m HEIGHT

(a)

1.75m HEIGHT ↔

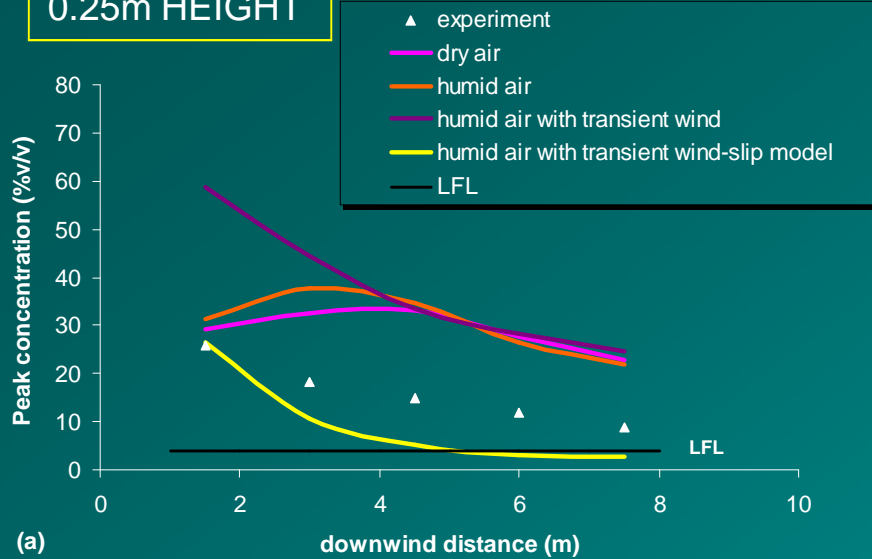


(b)

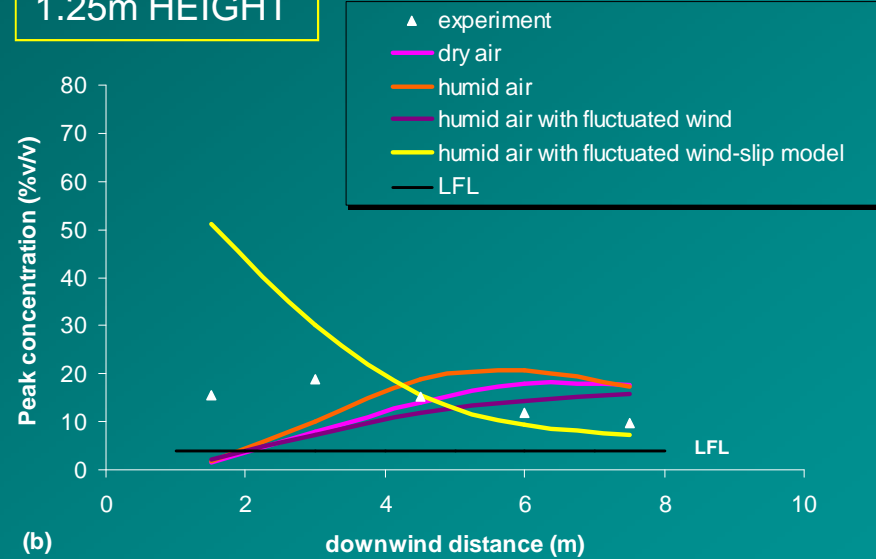


RESULTS (TEST 6)

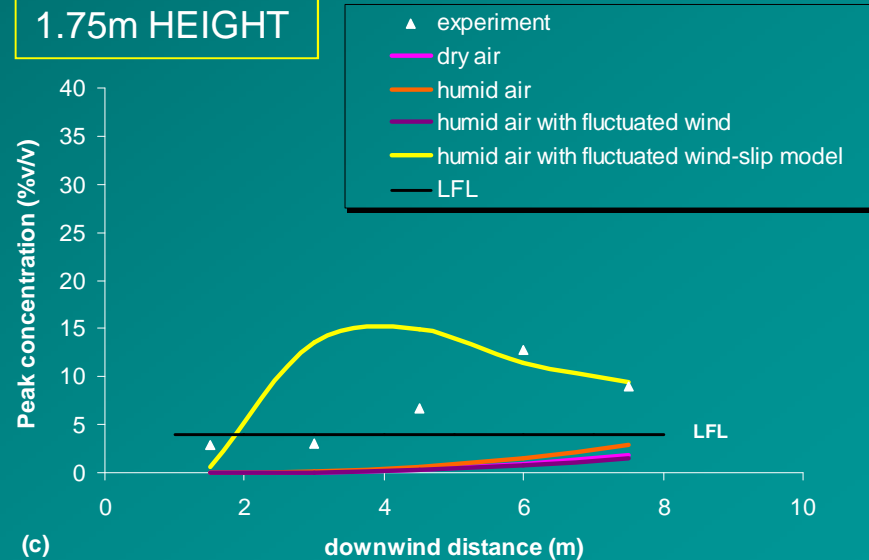
0.25m HEIGHT



1.25m HEIGHT



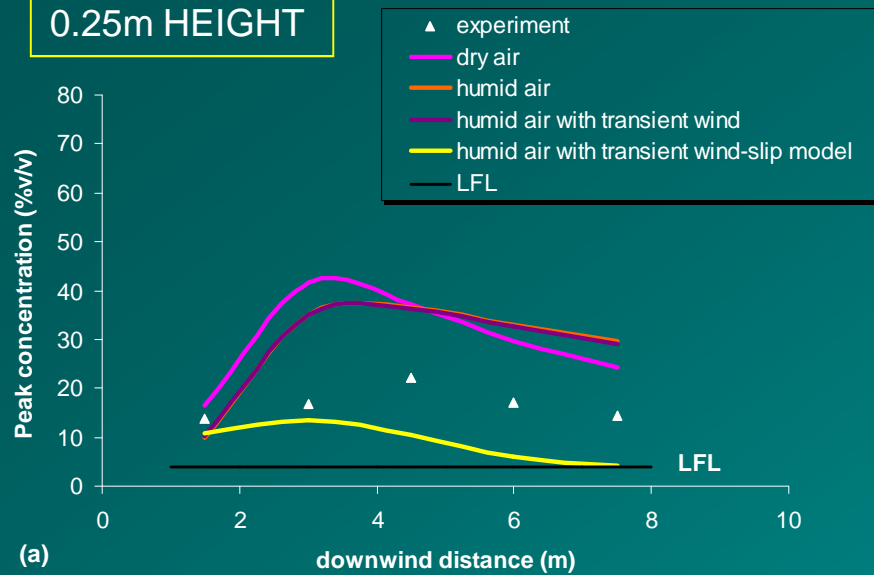
1.75m HEIGHT



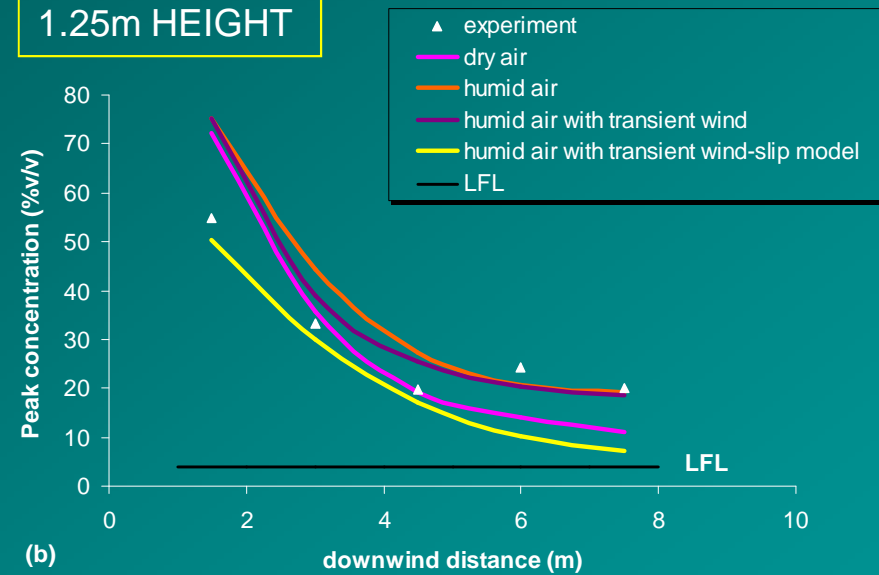


RESULTS (TEST 7)

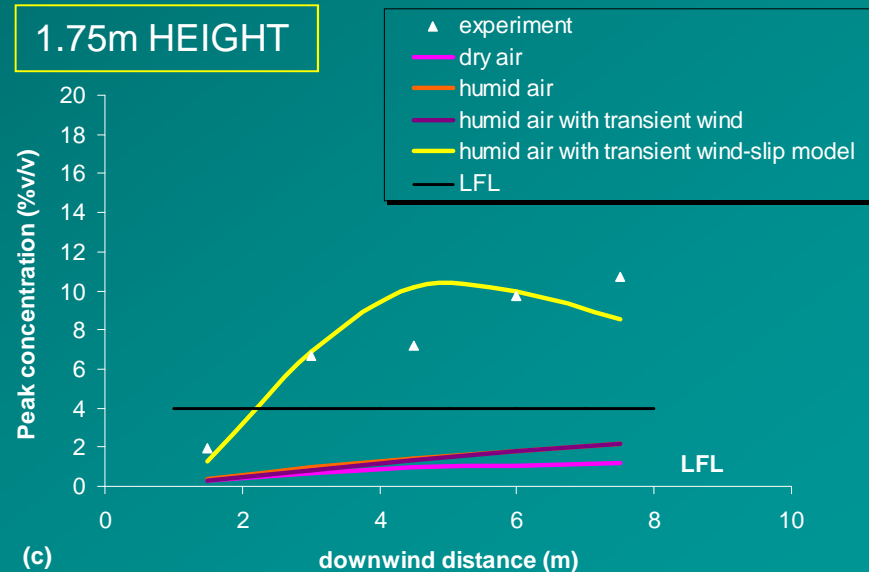
0.25m HEIGHT



1.25m HEIGHT



1.75m HEIGHT



* Yellow line is with coarse grid



CONCLUSIONS

- LH2 dispersion in open environment was simulated using HSL experiments
- Ambient humidity, wind direction, and slip effect were examined
- Humidity affects the dispersion. It makes the cloud more buoyant.
- Slip effect should be considered in two phase releases, especially when humidity is solved, in order to “see” the buoyancy effect.
- High wind direction fluctuations during large time intervals influence the course of the cloud.
 - When the calculation of the safety area is important wind direction is also important.
 - However, comparison with the maximum H2 concentrations in line with the release provide valuable information.
- The best simulation case (humidity + slip effect + transient wind direction) for test 5 and 6 is consistent with the experiment.
- For test 7 the cases without slip terms give underestimation for the H2 concentration at the higher sensors. Slip model improved the computational results even though a coarser grid was used.



FUTURE WORK

- Examination of slip effect in Test 7 with the fine grid.
- The air condensation (N_2 and O_2) and its effect on the prediction will be examined.
- Other slip models could be examined.
- Other wind profiles could be tested. A smoothing filter can be used.
- Heat flux from the ground to the cryogenic pool, using the boiling curve correlations will be implemented in ADREA-HF code and tested.

ANY QUESTIONS



THANK YOU FOR YOUR ATTENTION